Table 1 General Dowel Equation	ns
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$P = q_m \ell_m$			
	P = q	$m^{\ell}m$.	Main member bearing
$P = q_s \ell_s$	$P = 2q_s \ell_s$		Side member bearing
$P = \frac{-B + \sqrt{B^2 - 4AC}}{2A}$	$P=\frac{-B+}{}$	$\frac{\sqrt{B^2 - 4AC}}{A}$	General equation for member bearing and dowel yielding
	Inputs A, B, &	C for Yield Modes II-IV	
$A = \frac{1}{4q_s} + \frac{1}{4q_m}$	$B = \frac{\ell_s}{2} + g + \frac{\ell_m}{2}$	$C = -\frac{q_s \ell_s^2}{4} - \frac{q_m \ell_m^2}{4}$	Side and main member bearing
$A = \frac{1}{2q_s} + \frac{1}{4q_m}$	$B = g + \frac{\ell_m}{2}$	$C = -M_s - \frac{q_m \ell_m^2}{4}$	Main member bearing and dowel yielding in the side member
$A = \frac{1}{4q_s} + \frac{1}{2q_m}$	$B = \frac{\ell_s}{2} + g$	$C = -\frac{q_s \ell_s^2}{4} - M_m$	Side member bearing and dowel yielding in the main member
$A = \frac{1}{2q_s} + \frac{1}{2q_m}$	B = g	$C = -M_s - M_m$	Dowel yielding in the side and main member
	$P = q_s \ell_s$ $P = \frac{-B + \sqrt{B^2 - 4AC}}{2A}$ $A = \frac{1}{4q_s} + \frac{1}{4q_m}$ $A = \frac{1}{2q_s} + \frac{1}{4q_m}$ $A = \frac{1}{4q_s} + \frac{1}{2q_m}$ $A = \frac{1}{4q_s} + \frac{1}{2q_m}$ $A = \frac{1}{4q_s} + \frac{1}{2q_m}$	$P = q_s \ell_s$ $P = \frac{-B + \sqrt{B^2 - 4AC}}{2A}$ $P = \frac{-B + \sqrt{B^2 - 4AC}}{2A}$ $P = \frac{-B + \sqrt{B^2 - 4AC}}{2A}$ Inputs A, B, & $A = \frac{1}{4q_s} + \frac{1}{4q_m}$ $B = \frac{\ell_s}{2} + g + \frac{\ell_m}{2}$ $A = \frac{1}{2q_s} + \frac{1}{4q_m}$ $B = g + \frac{\ell_m}{2}$ $A = \frac{1}{4q_s} + \frac{1}{2q_m}$ $B = \frac{\ell_s}{2} + g$ $A = \frac{1}{4q_s} + \frac{1}{2q_m}$ $B = g$	$P = q_{s}\ell_{s}$ $P = \frac{1}{2} + \sqrt{B^{2} - 4AC}$ $P = \frac{1}{2} + \sqrt{B^{2} - 4AC}$ $P = \frac{1}{4} + \sqrt{B^{2} - 4AC}$ $P = \frac{1}{4} + \sqrt{B^{2} - 4AC}$ Inputs A, B, & C for Yield Modes II-IV $A = \frac{1}{4} + $

Notes:

P = nominal lateral connection value, lbs.

 $\ell_{\rm s}$ = side member dowel bearing length, in.

 $\ell_{\rm m}$ = main member dowel bearing length, in.

q_s = side member dowel-bearing resistance= F_{es}D, lbs./in.

q_m= main member dowel-bearing resistance= F_{em}D, lbs./in.

 F_{es} = side member dowel-bearing strength, psi

F_{em} = main member dowel-bearing strength, psi

g = gap between members, in.

D = dowel shank diameter, in.

 F_b = dowel bending strength, psi

 D_s = dowel diameter at max. stress in side member, in.

 D_m = dowel diameter at max. stress in main member, in.

 M_s = side member dowel moment resistance², in-lbs. = $F_b(D_s^3/6)$

 M_m = main member dowel moment resistance², in-lbs.= $F_b(D_m^3/6)$

Table 2 Reduction Terms Adjusting P_{5%} Values to Nominal Design Values

Fastener Type	Yield Mode	Reduction Term
Bolts, drift pins	$I_{\rm m}$, $I_{\rm s}$	4 K _θ
	Π	$3.6 K_{\theta}$
	III_m , III_s , IV	$3.2 K_{\theta}$
Lag screws	$I_{\rm m}^{\dagger}, I_{\rm s}$	$4 K_{\theta}$
	$\Pi^{\dagger},\Pi_{m}^{\dagger},\Pi_{s}$	$2.8 K_{\theta}$
	IV	$3 K_0$
Nails, spikes	I_m^{\dagger} , I_s , II_s , III_m , III_s , IV	$\mathbf{K}_{\mathbf{D}}$
Wood screws	$I_m^{\dagger}, I_s, \Pi^{\dagger}, \Pi I_m^{\dagger}, \Pi I_s, IV$	$\mathbf{K}_{\mathbf{D}}$
Notes:		
$K_{\theta} = 1 + 0.25(\theta/90)$	$K_{\rm D} = 2.2$	for D≤ 0.17"
θ = maximum angle of load to grain $(0^{\circ} \le \theta \le 90^{\circ})$	$K_D = 10D + 0.5$ for 0.17 " < D < 0.25 "	
for any member in a connection D = fastener shank diameter	$K_D = 3.0$	for D≥ 0.25"

[†]Yield modes and corresponding reduction terms are not provided in the NDS.



¹Yield Modes II and III_m are not applicable to double shear connections.

²For proportional limit values, $M_s = F_{b,pl}(\pi D_s^3/32)$ and $M_m = F_{b,pl}(\pi D_m^3/32)$.