	Length of nail	3.25 ii		dod states.	Load Duration Factor	1.6	
-	Nail diameter	0.135 ii		12d sinker			
-	Top of nail height	<b>1.50</b> ii	nches	See diagram	Wood species	Southern Pine	
	Thickness valley truss	1.50 ii	nches		Reference withdrawal unit strength	42 lbs/inch	
	Main truss slope Vertical component Horizontal component	5.50 12			Penetration for Lateral Strength Minimum penetration (6D)	0.81 inches	
	Slope angle, main truss Tan slope angle	24.6 c 0.458	degrees		Combined Withdrawa	al and Lateral Load (	per NDS-2005)
	Nail installation angle	<b>40</b> d	degrees		Alpha	50 degrees	\$2
	Tangent	0.839			Sine	0.766	
	Cosine	0.766			Cosine	0.643	
	Sine	0.643					
					Adjusted withdrawal capacity, W'p	76 lbs	
	Gap vertical	0.69 ii	nches		1 (14) 1 (15) (15) (16) (16) 16) (16) (16) (16) (16) (16) (16) (16)		
	Nail in upper truss, A	1.96 ir	nches	Ts			
	Wedge horizontal,B	1.26 ii	nches		Reference lateral capacity	89 lbs	per Technical Report 12
	C	1.70 ii	nches			75 da especiales	<ul> <li>■ Contract = 100 = 1000 (200) (2000 (200) (2000 (2000 (2000 (200) (2000 (2000 (200) (2000 (200) (2000 (200) (2000 (200) (2000 (200) (2000 (200) (2000 (200) (2000 (200) (2000 (200) (2000 (200) (2000 (200) (2000 (200) (2000 (200) (200) (200) (2000 (200) (200</li></ul>
	G2	0.57 ii	nches				
	Nail in gap, X	0.16 ii	nches	Χ	Adjusted lateral capacity, Z'	143 lbs	
	Nail penetration	1.14 ii	nches	Tm			
					Allowable inclined force, Z' alpha	69 lbs	
	Angle; nail & main truss	15.4 d	degrees				

Uplift Capacity As Toenail (Without Gap)

Nail penetration (without gap)

1.29 inches

Toenail withdrawal capacity

58 lbs

Toenail Factor

0.67

Calculation as toenail intended only as indirect "check" for upper part of nail in valley truss, assuming main truss in level position.

However, there is no code basis for such "check".

John F Mann, PE - 28070 Structural Support - COA 4216 1212 Main Street Belmar NJ 07719



Shaded cells are required inputs							A 4 A M								
	Nail Size: 12d			Nail Diameter, D		0.135 inches			Load is considered applied by side member to nail						
	Nail Type: Sir			Bending viel	nding yield strength of nail		100,000 psi								
Ivali Type. Oning					a saongar or nan	100,000 psi			Kd	2.2					
					Nail Length	3.25	inches								
Top of	Top of nail height installation angle	1.50	inches												
Nail installa		40	degrees		***	Side	<u>Main</u>		Re	1.0000					
	(Orang)	idas SAGES		Thic	ckness (inches)	1.96	3.50		Rt	0.58					
	Gap	0.16	inches												
				Dowel	Bearing Length	1.96	1.14								
					heta (degrees)	0	0		Thetamax	0					
ir	nput thickness	(side) & r	nail in nan	Theta (degrees)		0.000	0.000		Ktheta						
	nto Nail Shear	Daniel Or anno	C712 63		Sine Theta	0.00	0.00		Ruiota	1.00					
			p g		Cosine Theta	1.00	1.00		Theta =	Angle betw	veen direction of load				
										and direction of grain (long axis), for any member of connection					
					Species	SP	SP								
					West and the second sec	Part of the Part of State All Tables State Of the State O	CONTRACTOR				Total available length	5.61 inche	es		
					Specific Gravity	0.55	0.55								
				NTS 1 2013T-01 (F. 1931							Penetration, p				
				Dowel Bearing St	Section of the sectio	5,526	5,526		k1	0.347	Minimum penetration				
Dowel Bearing Strength, perpendic			i, perpendicular	5,526	5,526		k2	1.124		Based on nominal	diameter, D				
Carried Carrier Otherwalls				aarina Ctranath	E 506	E 500		k3	1.043	Manatoni'an fasta.	- 400 mu				
Dowel Bearing Strength <u>Tech Report 12</u>					5,526	5,526				Penetration factor	1.00 Eith	er 1 or 0			
Bending yield strength of nail; Fb,5% 100,000 psi											Load Duration Factor	1.00			
						NDS-2005					Wet Service Factor				
			Technical								Temperature Factor				
	*		Report 12	Least Z	Yield			Least Z		Ratio of	Group Action Factor	(A) A 20 (A)			
Α	В	С	Z (lbs)	Value	Mode	Rd	Z (lbs)	Value		Z Values	Geometry Factor	Van de saste an examena de la			
			385		1m	2.20	385		`	1.00	End Grain Factor	1.00			
	and the second		664	385	1s	2.20	664	385		1.00	Diaphragm Factor				
0.000670	1.703	-956	215	215	2	2.20	230	230		0.93	Toenail Factor	1.00			
0.001005	0.724	-282	127	127	3m	2.20	144	144		0.88					
0.001005	1.135	-756	214	127	3s	2.20	231	144		0.93	5.00				
0.001341	0.156	-82	89	89	4	2.20	112	112		0.79					
						a Lataval De	salan Malus	440	lla a		Unit withdrawal value	42 lbs pe	er inch of penetration		
				Keteren		ice Lateral Design Value Net Factor, Lateral		112 1.00	IDS		Net Factor, Withdrawa	1.00			
	Adjusted	l ateral D	esign Value	89 lbs		Netrac	ioi, Lateral	1,00			ivel racior, vvillidrawa	1.00			
	Adjusted	_utolal D	With gap		Δdinete	ted Lateral Design Value		112	lhe	Δ	Adjusted Withdrawal Design Value 47 lbs				
9			Author			English State Company of the Company			ina	^	ajustou vitituiawai Desigii value	47 lbs			
					For zero gap only										



## Wind Uplift Forces

Exposure							
Adjustment Factor	1.00		Adjustment Factor	1.00			
Tributary Area	8.00	sf	Tributary Area	8.00	sf		
Dead Load	3.00	psf	Dead Load	3.00	psf		
Main truss slope Vertical component Horizontal component	6 12		Main truss slope Vertical component Horizontal component	7 12			
Slope angle, main truss Tan slope angle Cosine	Tan slope angle 0.500		Slope angle, main truss Tan slope angle Cosine	30.26 0.583 0.864			
Zone Wind uplift pressure	1 27.8	2 48.4	Zone Wind uplift pressure	1 30.4	2 35.6		
Vertical wind uplift pressure Net wind uplift pressure Net wind uplift force	24.9 21.9 175	43.3 40.3 322	Vertical wind uplift pressure Net wind uplift pressure Net wind uplift force	26.3 23.3 186	30.8 27.8 222		

Wind uplift pressures per ASCE 7-05, components & cladding (Figure 6-3) Wind uplift pressure is applied perpencular ("normal") to roof surface

John F Mann, PE - 28070 Structural Support - COA 4216 1212 Main Street Belmar NJ 07719

